

## LMC6034 CMOS Quad Operational Amplifier

Check for Samples: [LMC6034](#)

### FEATURES

- Specified for 2 k $\Omega$  and 600 $\Omega$  Loads
- High Voltage Gain: 126 dB
- Low Offset Voltage Drift: 2.3  $\mu\text{V}/^\circ\text{C}$
- Ultra Low Input Bias Current: 40 fA
- Input Common-Mode Range Includes  $V^-$
- Operating Range from +5V to +15V Supply
- $I_{SS} = 400 \mu\text{A}/\text{Amplifier}$ ; Independent of  $V^+$
- Low Distortion: 0.01% at 10 kHz
- Slew Rate: 1.1 V/ $\mu\text{s}$
- Improved Performance Over TLC274

### DESCRIPTION

The LMC6034 is a CMOS quad operational amplifier which can operate from either a single supply or dual supplies. Its performance features include an input common-mode range that reaches ground, low input bias current, and high voltage gain into realistic loads, such as 2 k $\Omega$  and 600 $\Omega$ .

This chip is built with National's advanced Double-Poly Silicon-Gate CMOS process.

See the LMC6032 datasheet for a CMOS dual operational amplifier with these same features. For higher performance characteristics refer to the LMC660.

### APPLICATIONS

- High-Impedance Buffer or Preamplifier
- Current-to-Voltage Converter
- Long-Term Integrator
- Sample-and-Hold Circuit
- Medical Instrumentation

### Connection Diagram

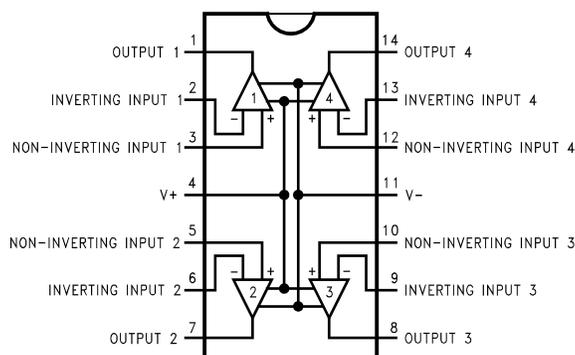
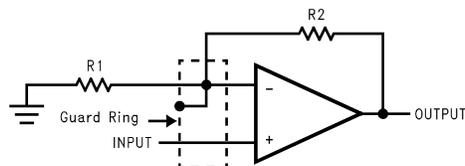


Figure 1. 14-Pin SOIC (Top View)

### Guard Ring Connections – Non-Inverting Amplifier



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These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

## ABSOLUTE MAXIMUM RATINGS<sup>(1)(2)</sup>

Differential Input Voltage	±Supply Voltage
Supply Voltage ( $V^+ - V^-$ )	16V
Output Short Circuit to $V^+$	See <sup>(3)</sup>
Output Short Circuit to $V^-$	See <sup>(4)</sup>
Lead Temperature (Soldering, 10 sec.)	260°C
Storage Temperature Range	-65°C to +150°C
Power Dissipation	See <sup>(5)</sup>
Voltage at Output/Input Pin	( $V^+$ ) +0.3V, ( $V^-$ ) -0.3V
Current at Output Pin	±18 mA
Current at Input Pin	±5 mA
Current at Power Supply Pin	35 mA
Junction Temperature <sup>(5)</sup>	150°C
ESD Tolerance <sup>(6)</sup>	1000V

- (1) Absolute Maximum Ratings indicate limits beyond which damage to the component may occur. Operating Ratings indicate conditions for which the device is intended to be functional, but do not guarantee specific performance limits. For guaranteed specifications and test conditions, see the Electrical Characteristics. The guaranteed specifications apply only for the test conditions listed.
- (2) If Military/Aerospace specified devices are required, please contact the TI Sales Office/ Distributors for availability and specifications.
- (3) Do not connect output to  $V^+$ , when  $V^+$  is greater than 13V or reliability may be adversely affected.
- (4) Applies to both single-supply and split-supply operation. Continuous short circuit operation at elevated ambient temperature and/or multiple Op Amp shorts can result in exceeding the maximum allowed junction temperature of 150°C. Output currents in excess of ±30 mA over long term may adversely affect reliability.
- (5) The maximum power dissipation is a function of  $T_{J(max)}$ ,  $\theta_{JA}$ ,  $T_A$ . The maximum allowable power dissipation at any ambient temperature is  $P_D = (T_{J(max)} - T_A) / \theta_{JA}$ .
- (6) Human body model, 100 pF discharged through a 1.5 kΩ resistor.

## OPERATING RATINGS<sup>(1)</sup>

Temperature Range	$-40^\circ\text{C} \leq T_J \leq +85^\circ\text{C}$	
Supply Voltage Range	4.75V to 15.5V	
Power Dissipation	See <sup>(2)</sup>	
Thermal Resistance ( $\theta_{JA}$ ) <sup>(3)</sup>	14-Pin SOIC	115°C/W

- (1) Absolute Maximum Ratings indicate limits beyond which damage to the component may occur. Operating Ratings indicate conditions for which the device is intended to be functional, but do not guarantee specific performance limits. For guaranteed specifications and test conditions, see the Electrical Characteristics. The guaranteed specifications apply only for the test conditions listed.
- (2) For operating at elevated temperatures the device must be derated based on the thermal resistance  $\theta_{JA}$  with  $P_D = (T_J - T_A) / \theta_{JA}$ .
- (3) All numbers apply for packages soldered directly into a PC board.

## DC ELECTRICAL CHARACTERISTICS

Unless otherwise specified, all limits guaranteed for  $T_J = 25^\circ\text{C}$ . **Boldface** limits apply at the temperature extremes.  $V^+ = 5\text{V}$ ,  $V^- = \text{GND} = 0\text{V}$ ,  $V_{CM} = 1.5\text{V}$ ,  $V_{OUT} = 2.5\text{V}$ , and  $R_L > 1\text{M}$  unless otherwise specified.

Symbol	Parameter	Conditions	Typical <sup>(1)</sup>	LMC6034I Limit <sup>(2)</sup>	Units
$V_{OS}$	Input Offset Voltage		1	9 <b>11</b>	mV max
$\Delta V_{OS}/\Delta T$	Input Offset Voltage Average Drift		2.3		$\mu\text{V}/^\circ\text{C}$
$I_B$	Input Bias Current		0.04	<b>200</b>	$\mu\text{A}$ max

- (1) Typical values represent the most likely parametric norm.
- (2) All limits are guaranteed at room temperature (standard type face) or at operating temperature extremes (**bold type face**).

**DC ELECTRICAL CHARACTERISTICS (continued)**

Unless otherwise specified, all limits guaranteed for  $T_J = 25^\circ\text{C}$ . **Boldface** limits apply at the temperature extremes.  $V^+ = 5\text{V}$ ,  $V^- = \text{GND} = 0\text{V}$ ,  $V_{\text{CM}} = 1.5\text{V}$ ,  $V_{\text{OUT}} = 2.5\text{V}$ , and  $R_L > 1\text{M}$  unless otherwise specified.

Symbol	Parameter	Conditions	Typical <sup>(1)</sup>	LMC6034I Limit <sup>(2)</sup>	Units
$I_{\text{OS}}$	Input Offset Current		0.01	<b>100</b>	pA max
$R_{\text{IN}}$	Input Resistance		>1		Tera $\Omega$
CMRR	Common Mode Rejection Ratio	$0\text{V} \leq V_{\text{CM}} \leq 12\text{V}$ $V^+ = 15\text{V}$	83	63 <b>60</b>	dB min
+PSRR	Positive Power Supply Rejection Ratio	$5\text{V} \leq V^+ \leq 15\text{V}$ $V_O = 2.5\text{V}$	83	63 <b>60</b>	dB min
-PSRR	Negative Power Supply Rejection Ratio	$0\text{V} \leq V^- \leq -10\text{V}$	94	74 <b>70</b>	dB min
$V_{\text{CM}}$	Input Common-Mode Voltage Range	$V^+ = 5\text{V} \ \& \ 15\text{V}$ For CMRR $\geq 50$ dB	-0.4	-0.1 <b>0</b>	V max
			$V^+ - 1.9$	$V^+ - 2.3$ <b><math>V^+ - 2.6</math></b>	V min
$A_V$	Large Signal Voltage Gain	$R_L = 2 \text{ k}\Omega^{(3)}$ Sourcing Sinking	2000	200 <b>100</b>	V/mV min
			500	90 <b>40</b>	V/mV min
		$R_L = 600\Omega^{(3)}$ Sourcing Sinking	1000	100 <b>75</b>	V/mV min
			250	50 <b>20</b>	V/mV min
$V_O$	Output Voltage Swing	$V^+ = 5\text{V}$ $R_L = 2 \text{ k}\Omega$ to 2.5V	4.87	4.20 <b>4.00</b>	V min
			0.10	0.25 <b>0.35</b>	V max
		$V^+ = 5\text{V}$ $R_L = 600\Omega$ to 2.5V	4.61	4.00 <b>3.80</b>	V min
			0.30	0.63 <b>0.75</b>	V max
		$V^+ = 15\text{V}$ $R_L = 2 \text{ k}\Omega$ to 7.5V	14.63	13.50 <b>13.00</b>	V min
			0.26	0.45 <b>0.55</b>	V max
		$V^+ = 15\text{V}$ $R_L = 600\Omega$ to 7.5V	13.90	12.50 <b>12.00</b>	V min
			0.79	1.45 <b>1.75</b>	V max

(3)  $V^+ = 15\text{V}$ ,  $V_{\text{CM}} = 7.5\text{V}$ , and  $R_L$  connected to 7.5V. For Sourcing tests,  $7.5\text{V} \leq V_O \leq 11.5\text{V}$ . For Sinking tests,  $2.5\text{V} \leq V_O \leq 7.5\text{V}$ .

## DC ELECTRICAL CHARACTERISTICS (continued)

Unless otherwise specified, all limits guaranteed for  $T_J = 25^\circ\text{C}$ . **Boldface** limits apply at the temperature extremes.  $V^+ = 5\text{V}$ ,  $V^- = \text{GND} = 0\text{V}$ ,  $V_{\text{CM}} = 1.5\text{V}$ ,  $V_{\text{OUT}} = 2.5\text{V}$ , and  $R_L > 1\text{M}$  unless otherwise specified.

Symbol	Parameter	Conditions	Typical <sup>(1)</sup>	LMC6034I Limit <sup>(2)</sup>	Units
$I_O$	Output Current	$V^+ = 5\text{V}$ Sourcing, $V_O = 0\text{V}$ Sinking, $V_O = 5\text{V}$	22	13 <b>9</b>	mA min
			21	13 <b>9</b>	mA min
		$V^+ = 15\text{V}$ Sourcing, $V_O = 0\text{V}$ Sinking, $V_O = 13\text{V}^{(4)}$	40	23 <b>15</b>	mA min
			39	23 <b>15</b>	mA min
$I_S$	Supply Current	All Four Amplifiers $V_O = 1.5\text{V}$	1.5	2.7 <b>3.0</b>	mA max

(4) Do not connect output to  $V^+$ , when  $V^+$  is greater than 13V or reliability may be adversely affected.

## AC ELECTRICAL CHARACTERISTICS

Unless otherwise specified, all limits guaranteed for  $T_J = 25^\circ\text{C}$ . **Boldface** limits apply at the temperature extremes.  $V^+ = 5\text{V}$ ,  $V^- = \text{GND} = 0\text{V}$ ,  $V_{\text{CM}} = 1.5\text{V}$ ,  $V_{\text{OUT}} = 2.5\text{V}$ , and  $R_L > 1\text{M}$  unless otherwise specified.

Symbol	Parameter	Conditions	Typical <sup>(1)</sup>	LMC6034I Limit <sup>(2)</sup>	Units
SR	Slew Rate	See <sup>(3)</sup>	1.1	0.8 <b>0.4</b>	V/ $\mu\text{s}$ min
GBW	Gain-Bandwidth Product		1.4		MHz
$\phi_M$	Phase Margin		50		Deg
$G_M$	Gain Margin		17		dB
	Amp-to-Amp Isolation	See <sup>(4)</sup>	130		dB
$e_n$	Input-Referred Voltage Noise	$F = 1\text{ kHz}$	22		nV/ $\sqrt{\text{Hz}}$
$i_n$	Input-Referred Current Noise	$F = 1\text{ kHz}$	0.0002		pA/ $\sqrt{\text{Hz}}$
THD	Total Harmonic Distortion	$F = 10\text{ kHz}$ , $A_V = -10$ $R_L = 2\text{ k}\Omega$ , $V_O = 8\text{ V}_{\text{PP}}$ $\pm 5\text{V}$ Supply	0.01		%

(1) Typical values represent the most likely parametric norm.

(2) All limits are guaranteed at room temperature (standard type face) or at operating temperature extremes (**bold type face**).

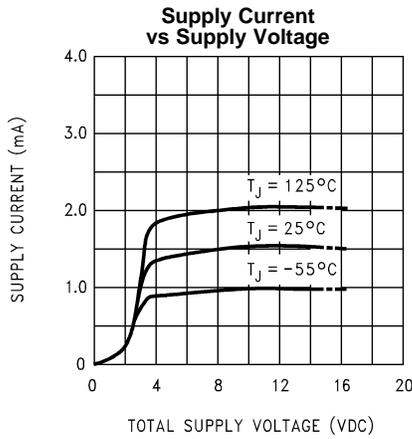
(3)  $V^+ = 15\text{V}$ . Connected as Voltage Follower with 10V step input. Number specified is the slower of the positive and negative slew rates.

(4) Input referred.  $V^+ = 15\text{V}$  and  $R_L = 10\text{ k}\Omega$  connected to  $V^+/2$ . Each amp excited in turn with 1 kHz to produce  $V_O = 13\text{ V}_{\text{PP}}$ .

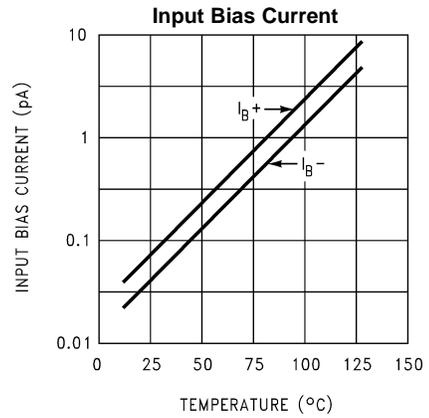
**TYPICAL PERFORMANCE CHARACTERISTICS**

$V_S = \pm 7.5V$ ,  $T_A = 25^\circ C$  unless otherwise specified

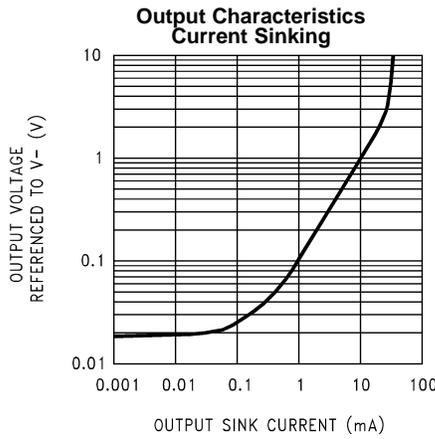
**Note:** Avoid resistive loads of less than 500Ω, as they may cause instability



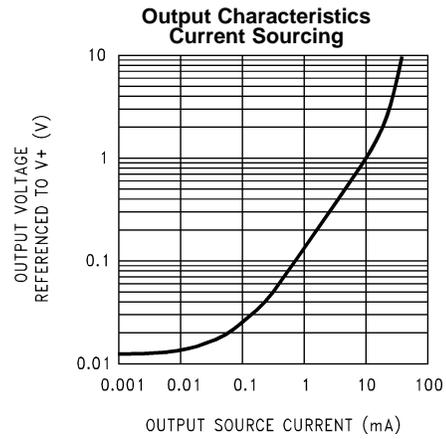
**Figure 2.**



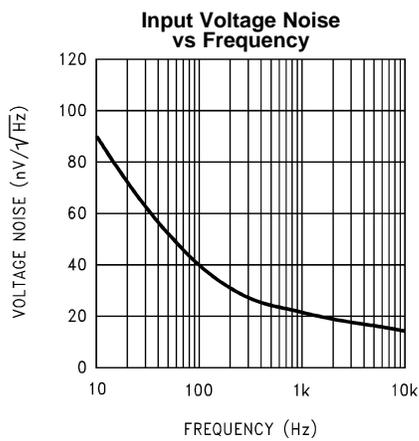
**Figure 3.**



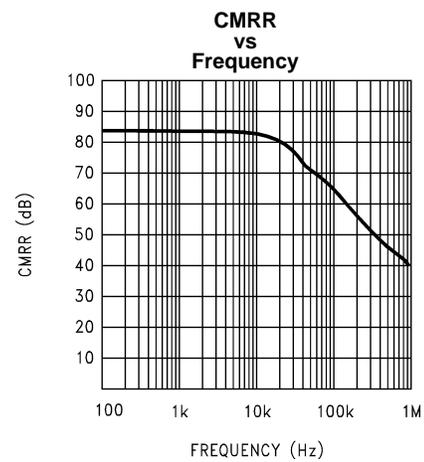
**Figure 4.**



**Figure 5.**



**Figure 6.**

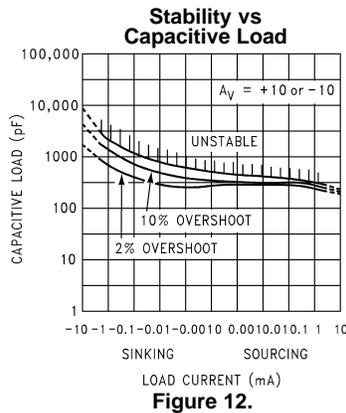
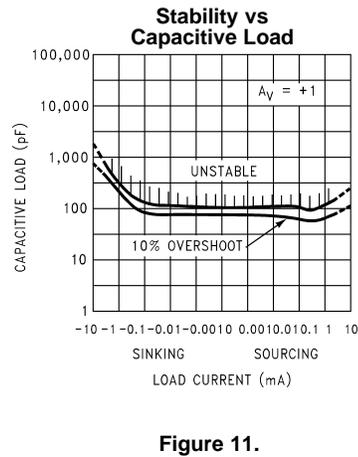
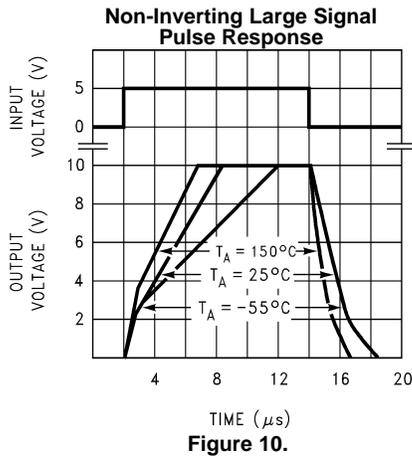
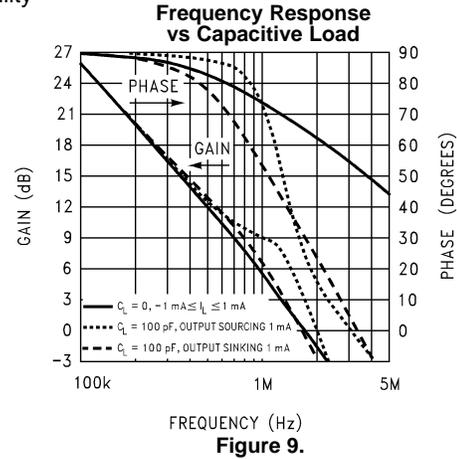
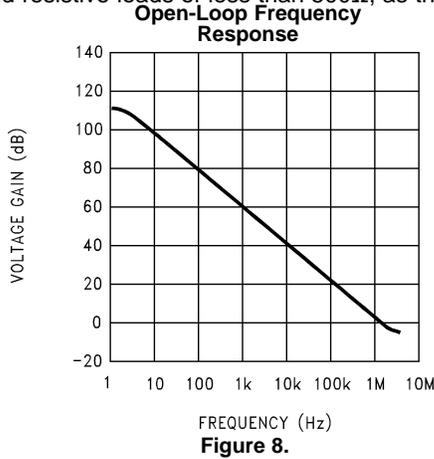


**Figure 7.**

**TYPICAL PERFORMANCE CHARACTERISTICS (continued)**

$V_S = \pm 7.5V$ ,  $T_A = 25^\circ C$  unless otherwise specified

**Note:** Avoid resistive loads of less than  $500\Omega$ , as they may cause instability



## APPLICATIONS HINT

### Amplifier Topology

The topology chosen for the LMC6034, shown in [Figure 13](#), is unconventional (compared to general-purpose op amps) in that the traditional unity-gain buffer output stage is not used; instead, the output is taken directly from the output of the integrator, to allow a larger output swing. Since the buffer traditionally delivers the power to the load, while maintaining high op amp gain and stability, and must withstand shorts to either rail, these tasks now fall to the integrator.

As a result of these demands, the integrator is a compound affair with an embedded gain stage that is doubly fed forward (via  $C_f$  and  $C_{ff}$ ) by a dedicated unity-gain compensation driver. In addition, the output portion of the integrator is a push-pull configuration for delivering heavy loads. While sinking current the whole amplifier path consists of three gain stages with one stage fed forward, whereas while sourcing the path contains four gain stages with two fed forward.

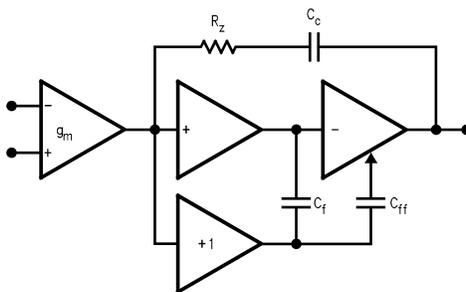


Figure 13. LMC6034 Circuit Topology (Each Amplifier)

The large signal voltage gain while sourcing is comparable to traditional bipolar op amps, even with a 600Ω load. The gain while sinking is higher than most CMOS op amps, due to the additional gain stage; however, under heavy load (600Ω) the gain will be reduced as indicated in the [Electrical Characteristics](#).

### Compensating Input Capacitance

The high input resistance of the LMC6034 op amps allows the use of large feedback and source resistor values without losing gain accuracy due to loading. However, the circuit will be especially sensitive to its layout when these large-value resistors are used.

Every amplifier has some capacitance between each input and AC ground, and also some differential capacitance between the inputs. When the feedback network around an amplifier is resistive, this input capacitance (along with any additional capacitance due to circuit board traces, the socket, etc.) and the feedback resistors create a pole in the feedback path. In the following [General Operational Amplifier circuit](#), the frequency of this pole is

$$f_p = \frac{1}{2\pi C_S R_P} \quad (1)$$

where  $C_S$  is the total capacitance at the inverting input, including amplifier input capacitance and any stray capacitance from the IC socket (if one is used), circuit board traces, etc., and  $R_P$  is the parallel combination of  $R_F$  and  $R_{IN}$ . This formula, as well as all formulae derived below, apply to inverting and non-inverting op-amp configurations.

When the feedback resistors are smaller than a few kΩ, the frequency of the feedback pole will be quite high, since  $C_S$  is generally less than 10 pF. If the frequency of the feedback pole is much higher than the “ideal” closed-loop bandwidth (the nominal closed-loop bandwidth in the absence of  $C_S$ ), the pole will have a negligible effect on stability, as it will add only a small amount of phase shift.

However, if the feedback pole is less than approximately 6 to 10 times the “ideal” –3 dB frequency, a feedback capacitor,  $C_F$ , should be connected between the output and the inverting input of the op amp. This condition can also be stated in terms of the amplifier’s low-frequency noise gain: To maintain stability a feedback capacitor will probably be needed if

$$\left(\frac{R_F}{R_{IN}} + 1\right) \leq \sqrt{6 \times 2\pi \times \text{GBW} \times R_F \times C_S} \quad (2)$$

where

$$\left(\frac{R_F}{R_{IN}} + 1\right) \quad (3)$$

is the amplifier's low-frequency noise gain and GBW is the amplifier's gain bandwidth product. An amplifier's low-frequency noise gain is represented by the formula

$$\left(\frac{R_F}{R_{IN}} + 1\right) \quad (4)$$

regardless of whether the amplifier is being used in inverting or non-inverting mode. Note that a feedback capacitor is more likely to be needed when the noise gain is low and/or the feedback resistor is large.

If the above condition is met (indicating a feedback capacitor will probably be needed), and the noise gain is large enough that:

$$\left(\frac{R_F}{R_{IN}} + 1\right) \geq 2\sqrt{\text{GBW} \times R_F \times C_S}, \quad (5)$$

the following value of feedback capacitor is recommended:

$$C_F = \frac{C_S}{2\left(\frac{R_F}{R_{IN}} + 1\right)} \quad (6)$$

If

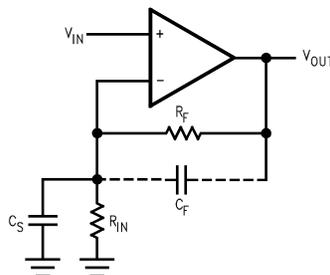
$$\left(\frac{R_F}{R_{IN}} + 1\right) < 2\sqrt{\text{GBW} \times R_F \times C_S} \quad (7)$$

the feedback capacitor should be:

$$C_F = \sqrt{\frac{C_S}{\text{GBW} \times R_F}} \quad (8)$$

Note that these capacitor values are usually significantly smaller than those given by the older, more conservative formula:

$$C_F = \frac{C_S R_{IN}}{R_F} \quad (9)$$



$C_S$  consists of the amplifier's input capacitance plus any stray capacitance from the circuit board and socket.  $C_F$  compensates for the pole caused by  $C_S$  and the feedback resistors.

**Figure 14. General Operational Amplifier Circuit**

Using the smaller capacitors will give much higher bandwidth with little degradation of transient response. It may be necessary in any of the above cases to use a somewhat larger feedback capacitor to allow for unexpected stray capacitance, or to tolerate additional phase shifts in the loop, or excessive capacitive load, or to decrease the noise or bandwidth, or simply because the particular circuit implementation needs more feedback capacitance to be sufficiently stable. For example, a printed circuit board's stray capacitance may be larger or smaller than the breadboard's, so the actual optimum value for  $C_F$  may be different from the one estimated using the breadboard. In most cases, the values of  $C_F$  should be checked on the actual circuit, starting with the computed value.

### Capacitive Load Tolerance

Like many other op amps, the LMC6034 may oscillate when its applied load appears capacitive. The threshold of oscillation varies both with load and circuit gain. The configuration most sensitive to oscillation is a unity-gain follower. See [Typical Performance Characteristics](#).

The load capacitance interacts with the op amp's output resistance to create an additional pole. If this pole frequency is sufficiently low, it will degrade the op amp's phase margin so that the amplifier is no longer stable at low gains. As shown in [Figure 15](#), the addition of a small resistor ( $50\Omega$  to  $100\Omega$ ) in series with the op amp's output, and a capacitor ( $5\text{ pF}$  to  $10\text{ pF}$ ) from inverting input to output pins, returns the phase margin to a safe value without interfering with lower-frequency circuit operation. Thus larger values of capacitance can be tolerated without oscillation. Note that in all cases, the output will ring heavily when the load capacitance is near the threshold for oscillation.

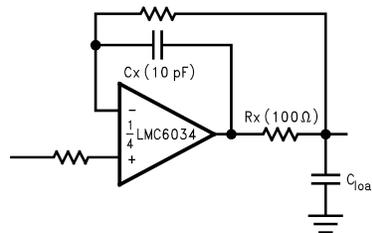


Figure 15. Rx, Cx Improve Capacitive Load Tolerance

Capacitive load driving capability is enhanced by using a pull up resistor to  $V^+$  ([Figure 16](#)). Typically a pull up resistor conducting  $500\ \mu\text{A}$  or more will significantly improve capacitive load responses. The value of the pull up resistor must be determined based on the current sinking capability of the amplifier with respect to the desired output swing. Open loop gain of the amplifier can also be affected by the pull up resistor (see [Electrical Characteristics](#)).

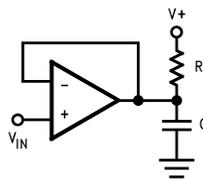
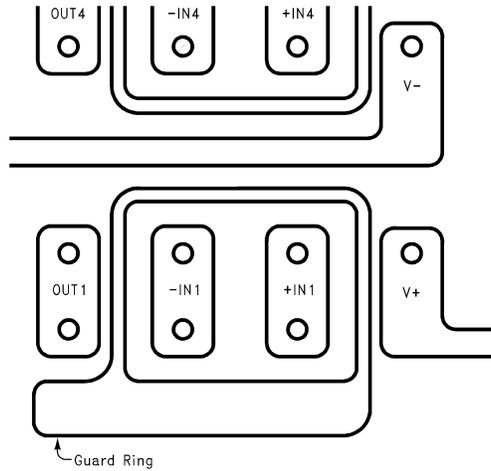


Figure 16. Compensating for Large Capacitive Loads with a Pull Up Resistor

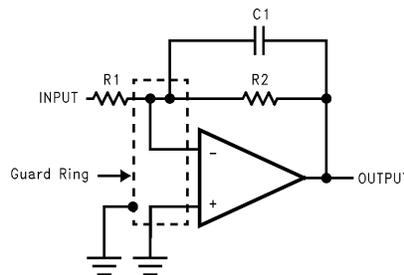
### PRINTED-CIRCUIT-BOARD LAYOUT FOR HIGH-IMPEDANCE WORK

It is generally recognized that any circuit which must operate with less than  $1000\text{ pA}$  of leakage current requires special layout of the PC board. When one wishes to take advantage of the ultra-low bias current of the LMC6034, typically less than  $0.04\text{ pA}$ , it is essential to have an excellent layout. Fortunately, the techniques for obtaining low leakages are quite simple. First, the user must not ignore the surface leakage of the PC board, even though it may sometimes appear acceptably low, because under conditions of high humidity or dust or contamination, the surface leakage will be appreciable.

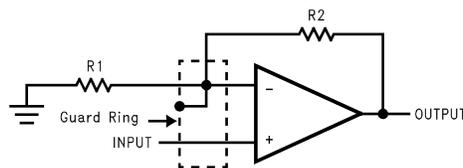
To minimize the effect of any surface leakage, lay out a ring of foil completely surrounding the LMC6034's inputs and the terminals of capacitors, diodes, conductors, resistors, relay terminals, etc. connected to the op-amp's inputs. See [Figure 17](#) . To have a significant effect, guard rings should be placed on both the top and bottom of the PC board. This PC foil must then be connected to a voltage which is at the same voltage as the amplifier inputs, since no leakage current can flow between two points at the same potential. For example, a PC board trace-to-pad resistance of  $10^{12}\Omega$ , which is normally considered a very large resistance, could leak 5 pA if the trace were a 5V bus adjacent to the pad of an input. This would cause a 100 times degradation from the LMC6034's actual performance. However, if a guard ring is held within 5 mV of the inputs, then even a resistance of  $10^{11}\Omega$  would cause only 0.05 pA of leakage current, or perhaps a minor (2:1) degradation of the amplifier's performance. See [Figure 18](#), [Figure 19](#) and , [Figure 20](#) for typical connections of guard rings for standard op-amp configurations. If both inputs are active and at high impedance, the guard can be tied to ground and still provide some protection; see [Figure 21](#).



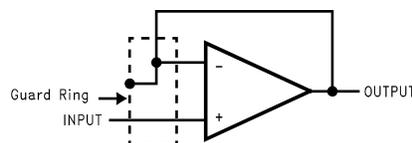
**Figure 17. Example of Guard Ring in P.C. Board Layout**



**Figure 18. Guard Ring Connections Inverting Amplifier**



**Figure 19. Guard Ring Connections Non-Inverting Amplifier**



**Figure 20. Guard Ring Connections Follower**

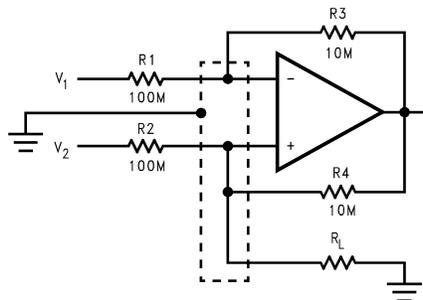
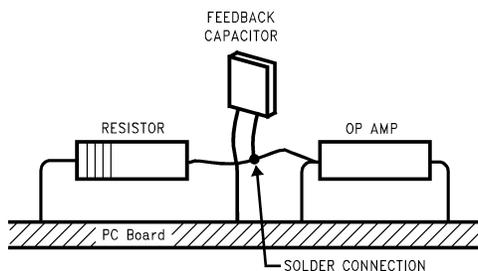


Figure 21. Guard Ring Connections Howland Current Pump

The designer should be aware that when it is inappropriate to lay out a PC board for the sake of just a few circuits, there is another technique which is even better than a guard ring on a PC board: Don't insert the amplifier's input pin into the board at all, but bend it up in the air and use only air as an insulator. Air is an excellent insulator. In this case you may have to forego some of the advantages of PC board construction, but the advantages are sometimes well worth the effort of using point-to-point up-in-the-air wiring. See Figure 22.



(Input pins are lifted out of PC board and soldered directly to components. All other pins connected to PC board.)

Figure 22. Air Wiring

### BIAS CURRENT TESTING

The test method of Figure 23 is appropriate for bench-testing bias current with reasonable accuracy. To understand its operation, first close switch S2 momentarily. When S2 is opened, then

$$I_{b^-} = \frac{dV_{OUT}}{dt} \times C2. \tag{10}$$

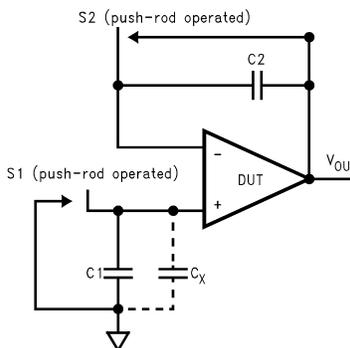


Figure 23. Simple Input Bias Current Test Circuit

A suitable capacitor for C2 would be a 5 pF or 10 pF silver mica, NPO ceramic, or air-dielectric. When determining the magnitude of  $I_{b^-}$ , the leakage of the capacitor and socket must be taken into account. Switch S2 should be left shorted most of the time, or else the dielectric absorption of the capacitor C2 could cause errors.

Similarly, if S1 is shorted momentarily (while leaving S2 shorted)

$$I_b^+ = \frac{dV_{OUT}}{dt} \times (C_1 + C_x) \tag{11}$$

where  $C_x$  is the stray capacitance at the + input.

### Typical Single-Supply Applications

( $V^+ = 5.0$  VDC)

Additional single-supply applications ideas can be found in the LM324 datasheet. The LMC6034 is pin-for-pin compatible with the LM324 and offers greater bandwidth and input resistance over the LM324. These features will improve the performance of many existing single-supply applications. Note, however, that the supply voltage range of the LMC6034 is smaller than that of the LM324.

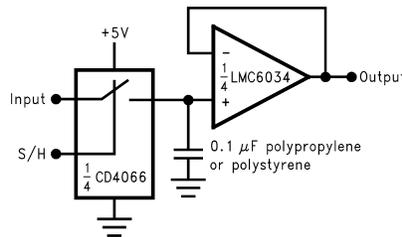


Figure 24. Low-Leakage Sample-and-Hold

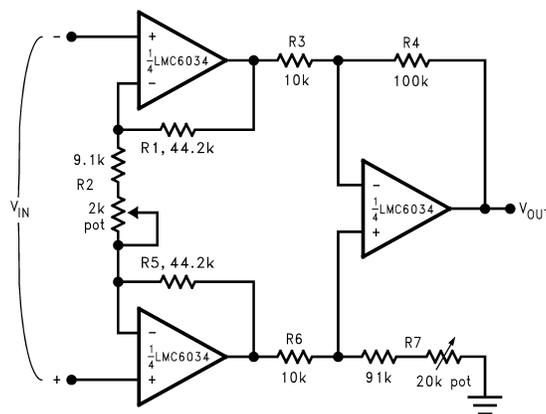


Figure 25. Instrumentation Amplifier

$$\frac{V_{OUT}}{V_{IN}} = \frac{R_2 + 2R_1}{R_2} \times \frac{R_4}{R_3} \tag{12}$$

if  $R_1 = R_5$

$R_3 = R_6$ .

and  $R_4 = R_7$ .

$$\frac{V_{OUT}}{V_{IN}} = 100 \text{ for circuit as shown.} \tag{13}$$

For good CMRR over temperature, low drift resistors should be used. Matching of  $R_3$  to  $R_6$  and  $R_4$  to  $R_7$  affect CMRR. Gain may be adjusted through  $R_2$ . CMRR may be adjusted through  $R_7$ .

(V<sup>+</sup> = 5.0 VDC)

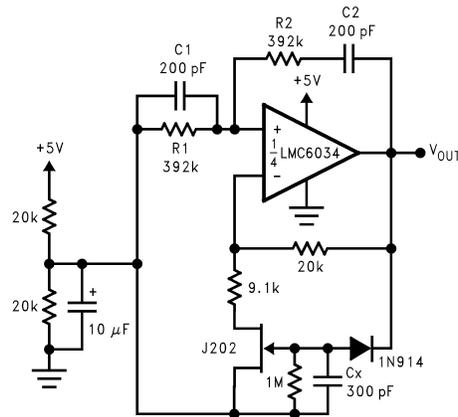


Figure 26. Sine-Wave Oscillator

Oscillator frequency is determined by R1, R2, C1, and C2:

$$f_{osc} = 1/2\pi RC, \text{ where } R = R1 = R2 \text{ and } C = C1 = C2.$$

This circuit, as shown, oscillates at 2.0 kHz with a peak-to-peak output swing of 4.0V.

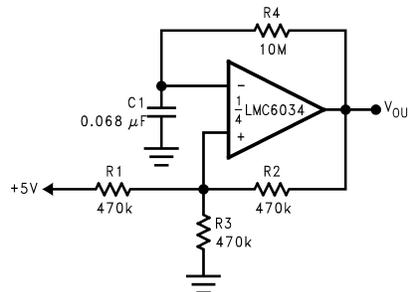


Figure 27. 1 Hz Square-Wave Oscillator

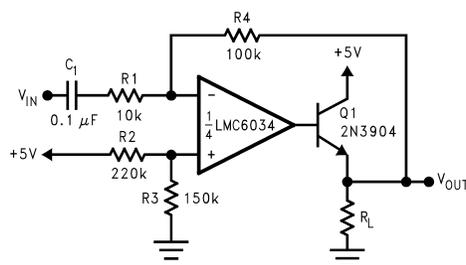
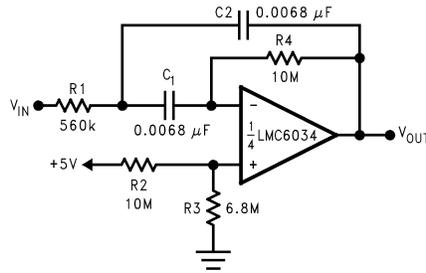


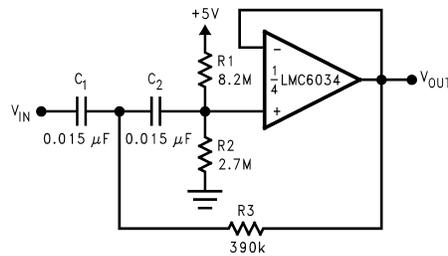
Figure 28. Power Amplifier

(V<sup>+</sup> = 5.0 VDC)



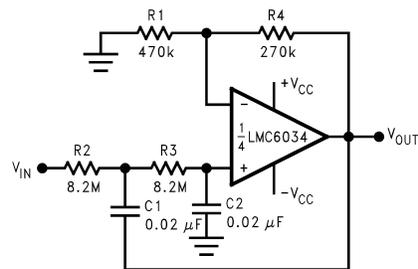
f<sub>0</sub> = 10 Hz  
 Q = 2.1  
 Gain = -8.8

Figure 29. 10 Hz Bandpass Filter



f<sub>c</sub> = 10 Hz  
 d = 0.895  
 Gain = 1  
 2 dB passband ripple

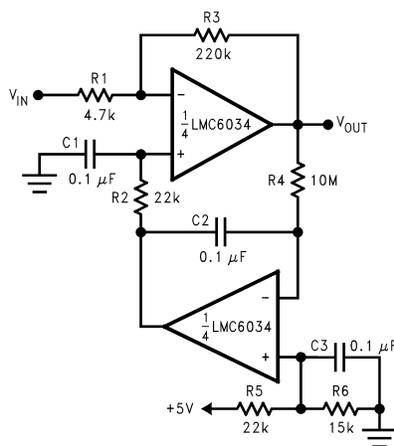
Figure 30. 10 Hz High-Pass Filter



f<sub>c</sub> = 1 Hz  
 d = 1.414  
 Gain = 1.57

Figure 31. 1 Hz Low-Pass Filter (Maximally Flat, Dual Supply Only)

(V<sup>+</sup> = 5.0 VDC)



Gain = -46.8

Output offset voltage reduced to the level of the input offset voltage of the bottom amplifier (typically 1 mV).

**Figure 32. High Gain Amplifier with Offset Voltage Reduction**

## REVISION HISTORY

Changes from Revision B (March 2013) to Revision C	Page
• Changed layout of National Data Sheet to TI format .....	<a href="#">15</a>

## PACKAGING INFORMATION

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead/Ball Finish	MSL Peak Temp (3)	Op Temp (°C)	Top-Side Markings (4)	Samples
LMC6034IM	ACTIVE	SOIC	D	14	55	TBD	Call TI	Call TI	-40 to 85	LMC6034IM	<a href="#">Samples</a>
LMC6034IM/NOPB	ACTIVE	SOIC	D	14	55	Green (RoHS & no Sb/Br)	CU SN	Level-1-260C-UNLIM	-40 to 85	LMC6034IM	<a href="#">Samples</a>
LMC6034IMX	ACTIVE	SOIC	D	14	2500	TBD	Call TI	Call TI	-40 to 85	LMC6034IM	<a href="#">Samples</a>
LMC6034IMX/NOPB	ACTIVE	SOIC	D	14	2500	Green (RoHS & no Sb/Br)	CU SN	Level-1-260C-UNLIM	-40 to 85	LMC6034IM	<a href="#">Samples</a>

(1) The marketing status values are defined as follows:

**ACTIVE:** Product device recommended for new designs.

**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW:** Device has been announced but is not in production. Samples may or may not be available.

**OBSOLETE:** TI has discontinued the production of the device.

(2) Eco Plan - The planned eco-friendly classification: Pb-Free (RoHS), Pb-Free (RoHS Exempt), or Green (RoHS & no Sb/Br) - please check <http://www.ti.com/productcontent> for the latest availability information and additional product content details.

**TBD:** The Pb-Free/Green conversion plan has not been defined.

**Pb-Free (RoHS):** TI's terms "Lead-Free" or "Pb-Free" mean semiconductor products that are compatible with the current RoHS requirements for all 6 substances, including the requirement that lead not exceed 0.1% by weight in homogeneous materials. Where designed to be soldered at high temperatures, TI Pb-Free products are suitable for use in specified lead-free processes.

**Pb-Free (RoHS Exempt):** This component has a RoHS exemption for either 1) lead-based flip-chip solder bumps used between the die and package, or 2) lead-based die adhesive used between the die and leadframe. The component is otherwise considered Pb-Free (RoHS compatible) as defined above.

**Green (RoHS & no Sb/Br):** TI defines "Green" to mean Pb-Free (RoHS compatible), and free of Bromine (Br) and Antimony (Sb) based flame retardants (Br or Sb do not exceed 0.1% by weight in homogeneous material)

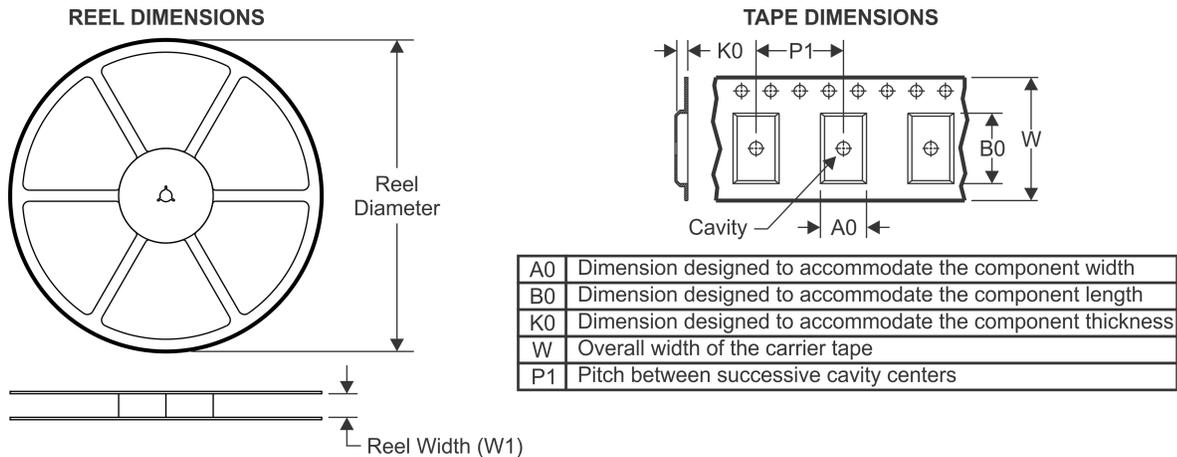
(3) MSL, Peak Temp. -- The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

(4) Only one of markings shown within the brackets will appear on the physical device.

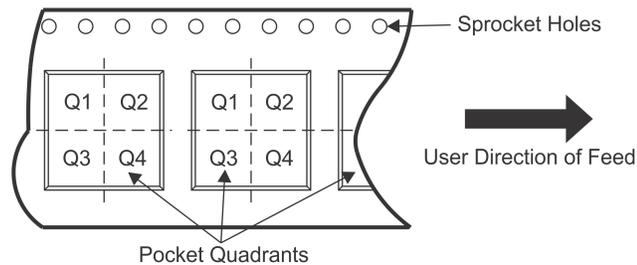
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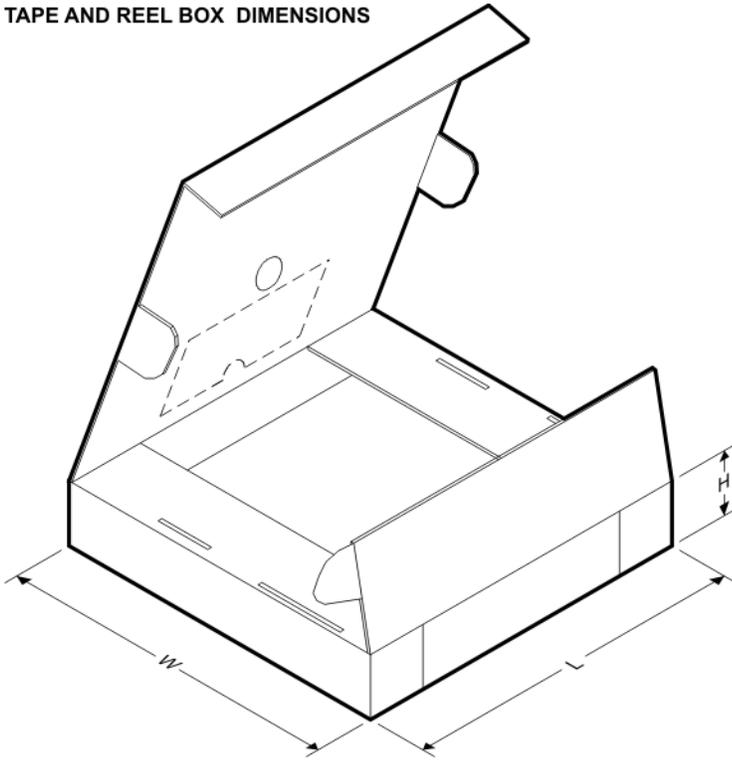
### QUADRANT ASSIGNMENTS FOR PIN 1 ORIENTATION IN TAPE



\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Reel Diameter (mm)	Reel Width W1 (mm)	A0 (mm)	B0 (mm)	K0 (mm)	P1 (mm)	W (mm)	Pin1 Quadrant
LMC6034IMX	SOIC	D	14	2500	330.0	16.4	6.5	9.35	2.3	8.0	16.0	Q1
LMC6034IMX/NOPB	SOIC	D	14	2500	330.0	16.4	6.5	9.35	2.3	8.0	16.0	Q1

TAPE AND REEL BOX DIMENSIONS

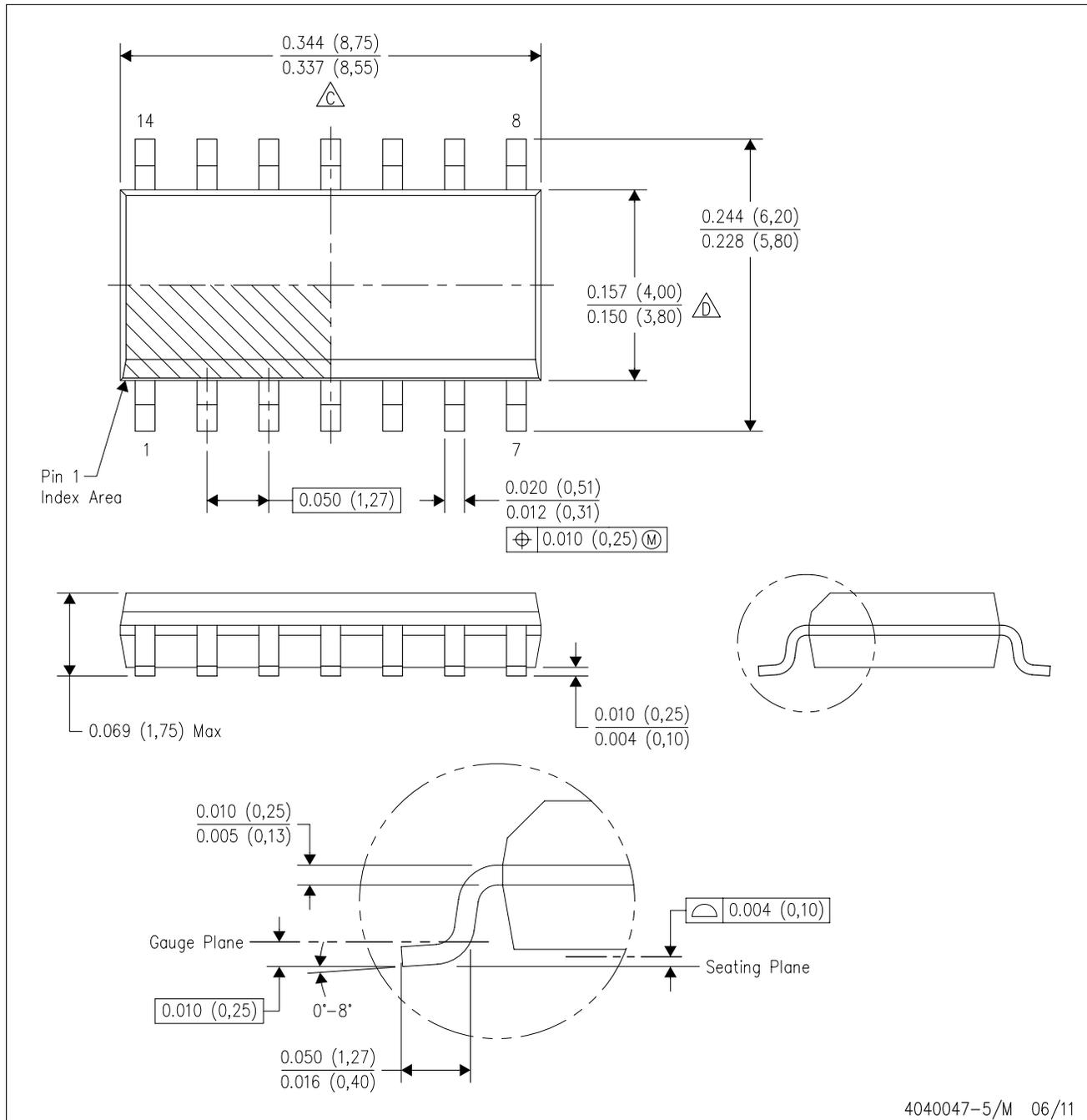


\*All dimensions are nominal

Device	Package Type	Package Drawing	Pins	SPQ	Length (mm)	Width (mm)	Height (mm)
LMC6034IMX	SOIC	D	14	2500	349.0	337.0	45.0
LMC6034IMX/NOPB	SOIC	D	14	2500	349.0	337.0	45.0

D (R-PDSO-G14)

PLASTIC SMALL OUTLINE



- NOTES:
- A. All linear dimensions are in inches (millimeters).
  - B. This drawing is subject to change without notice.
  -  Body length does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed 0.006 (0,15) each side.
  -  Body width does not include interlead flash. Interlead flash shall not exceed 0.017 (0,43) each side.
  - E. Reference JEDEC MS-012 variation AB.

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